

Manipal Institute of Technology, Manipal

(A Constituent Institute of Manipal University)

## SEVENTH SEMESTER B.TECH (INSTRUMENTATION & CONTROL ENGINEERING) END SEMESTER EXAMINATIONS, NOV/DEC 2015

SUBJECT: ROBUST CONTROL [ICE 439]

Time: 3 Hours

MAX. MARKS: 50

(02)

## Instructions to Candidates:

- ✤ Answer ANY FIVE FULL questions.
- ✤ Missing data may be suitably assumed.

1A. Find the corresponding state space model of the system  $G(s) = \frac{1}{s^2+s+1}$  and calculate (08)  $\|G\|_2$  via state space method. Also obtained the  $\infty$ -norm of the system.

- **1B.** Illustrate parametric uncertainty in plant model with example.
- 2A. A plant has transfer function  $G(s) = e^{-sd} \frac{1}{s^2+0.4s+1}$ . The delay *d* is unknown, but lies (05) between 0 and 4. A proportional feedback controller is implemented with gain *K*. Use small gain theorem to determine the maximum gain *K* that preserves the stability for all possible values of *d* and also interpret your answer in terms of the Nyquist criterion.
- 2B. Assume that unity feedback system as shown in Fig. Q (2B) is internally stable and n = (03) d = 0. Show that if input r(t) is the unit step than  $e(t) \rightarrow 0$  as  $t \rightarrow \infty$  if and only if sensitivity transfer function S(s) has at least one zero at the origin.



Fig. Q(2B)

2C. Interpret graphically the norm bound performance condition  $||W_P(s)S(s)||_{\infty} < 1$  for (02) the feedback control system.

- 3A. Design a controller *C* for the plant model  $P(s) = \frac{3}{s-4}$  of unity feedback system as (08) shown in Fig. Q(2B) so that tracking error *e* goes to 0, when *r* is a ramp and n = d = 0.
- **3B.** Show that set of all controllers of plant  $P \in R\mathcal{H}_{\infty}$  for which the feedback system (02) shown in Fig. Q(2B) is internally stable is given by  $C = \left\{ \frac{Q}{1-PQ} : Q \in R\mathcal{H}_{\infty} \right\}$
- 4. Establish the necessary and sufficient condition for robust performance in the feedback (10) control system.
- 5A. Consider  $P(s) = \frac{1}{s}$  and  $W_P(s) = \frac{100}{s+1}$ . Perturb P to  $P(s) = 1/(s+\epsilon)$ ,  $\epsilon > 0$ . Find (05) the controller C (internally stabilizing) so that  $||W_PS||_{\infty} < 1$ . Does the resulting controller C solve the performance design problem for the original P?
- **5B.** Factor **P** as  $P = P_1P_2$ ,  $P_1 = \frac{1}{s+1}$ ,  $P_2 = \frac{s+1}{s}$ . Solve the performance design problem (05) for **P**<sub>1</sub>; let **C**<sub>1</sub> be the solution. Set **C** = **C**<sub>1</sub>/**P**<sub>2</sub>. Does the resulting **C** solve the performance design problem for the original **P**? If so, explain why.
- 6A. Open-loop plant P(s) is strictly proper, has a double pole at s = 0, and a zero at s = (05)
  0.1. Controller C = C(s) stabilizes the feedback system shown in Fig. Q6(A) and ensures good tracking (transfer function from r to e has gain less than 0.1) for frequencies up to 1 rad/sec. Find a good lower bound on the maximal gain from r to e.



Fig. Q6(A)

6B. Suppose G is stable and G(0) is non-singular. For the loop in Fig. Q6(B), find all (05) stabilizing controllers such that the steady-state value of y is zero when v is a step input and w = 0.



**Fig. Q6(B)**