Reg.No.

MANIPAL INSTITUTE OF TECHNOLOGY

(A constituent unit of MAHE, Manipal)

FIRST SEMESTER M.TECH. (CONTROL SYSTEMS AND AEROSPACE ENGG.)

END SEMESTER EXAMINATIONS, NOVEMBER - 2018

ADVANCED CONTROL SYSTEMS [ICE 5102]

TIME: 3 Hour

Instructions to candidates:

- Answer **ALL** questions.
- Missing data may be suitably assumed.
- 1A Enumerate the design philosophy of Lag compensator using Frequency response.
- **1B** Correlate the time response specification and frequency response specification for a second 3 order system. Hence derive the expression for phase margin and gain cross over frequency in terms of damping ratio and natural frequency.
- **1C** A unity feedback system has the transfer function

 $G_p(s) = \frac{4}{s(s+2)}$. Design a Lead compensator to place the closed loop poles to satisfy a

damping ratio of 0.5 and natural frequency of 4 rad/sec. Also determine additional gain if any necessary.

- 2A List the advantages of state variable method of analysis compared to conventional method. 2
- **2B** The state equations of a system are as follows:

$$\begin{vmatrix} \dot{x}_{1}(t) \\ \dot{x}_{2}(t) \\ \dot{x}_{3}(t) \end{vmatrix} = \begin{vmatrix} -4 & 1 & 0 \\ 0 & -3 & 0 \\ 0 & 0 & -1 \end{vmatrix} \begin{vmatrix} x_{1}(t) \\ x_{2}(t) \\ x_{3}(t) \end{vmatrix} + \begin{vmatrix} 0 \\ 2 \\ 2 \end{vmatrix} u(t)$$

- i) Determine the eigen values
- ii) Determine a transformation matrix V which uncouples the states.
- iii) Determine a transformation matrix P, which transforms system matrix into controllable canonical form.
- **2C** Consider the system whose state and output equations are given as

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ -1 & -1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

- i) Obtain the transfer function.
- ii) From the nature of transfer function and state model, comment on nature of



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MAX. MARKS:50

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realization and controllability and observability property.

3A For the system described by

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 2 \\ 0 & -4 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 1 \\ 2 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

Determine the state transition matrix using Cayley-Hamilton method. Hence determine the zero initial state and unit step input response for $x_1(t)$ and $x_2(t)$. Realize the digital controller defined by

3B

$$G(z) = \frac{U(z)}{E(z)} = \frac{4(z-1)(z^2+1.2z+1)}{(z+0.1)(z^2-0.3z+0.8)},$$
 in cascade form.

3C Obtain the state model for the following difference equation y(k+2)+3y(k+1)+2y(k)=0

Using the initial condition, $y(-1) = -\frac{1}{2}$, $y(-2) = \frac{3}{4}$, determine $x_1(0)$ and $x_2(0)$. Hence solve for

y(k) using z transform method.

Derive expressions for obtaining a discrete time state model from a given continuous time state **4**A 5 model. Hence obtain the discrete time state model for the system described in Q(3A)considering the sampling time as T=0.2 seconds. 5

4B For the plant represented by

 $\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -2 & -4 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u(t), \text{ design a state feedback matrix K, that assigns the set of}$

closed loop plant eigen values as [-3, -6] by direct method and using Ackerman's formula.

- **5**A What is an observer? Derive the design formula for a full order observer. Show that the same is 5 dual to state feedback control design and comment on the result. 3
- Consider a plant described by the following state variable model **5B**

$$\begin{bmatrix} x_{1}(k+1) \\ x_{2}(k+1) \\ x_{3}(k+1) \end{bmatrix} = \begin{bmatrix} \frac{1}{2} & 1 & 0 \\ -1 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_{1}(k) \\ x_{2}(k) \\ x_{3}(k) \end{bmatrix} + \begin{bmatrix} 1 & 4 \\ 0 & 0 \\ -3 & 2 \end{bmatrix} \begin{bmatrix} u_{1}(k) \\ u_{2}(k) \end{bmatrix}$$
$$Y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_{1}(k) \\ x_{2}(k) \\ x_{3}(k) \end{bmatrix} + \begin{bmatrix} 0 & 4 \end{bmatrix} \begin{bmatrix} u_{1}(k) \\ u_{2}(k) \end{bmatrix}$$

Design a full order observer for the estimation of the state vector X; the observer error poles are required to be at $-\frac{1}{2} \pm j\frac{1}{4}$,0.

5C What is dead beat control by state feedback and dead beat observers? 2

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