**IANIPAL INSTITUTE OF TECHNOLOGY** 

(A constituent unit of MAHE, Manipal)

## SEVENTH SEMESTER B.TECH. (INSTRUMENTATION AND CONTROL ENGG.) END SEMESTER DEGREE EXAMINATIONS, NOVEMBER - 2019

SUBJECT: ROBOTIC SYSTEMS AND CONTROL [ICE 4030]

## TIME: 3 HOURS

## MAX. MARKS: 50

## Instructions to candidates : Answer ALL questions and missing data may be suitably assumed.

- 1A. Determine the degrees of freedom for the mechanism shown in Fig. Q1A.
- 1B. The end-point of a link of a manipulator is at  $P_1 = [2 \ 2 \ 6]^T$  w.r.t a global frame of reference  $O_1XYZ$ . Assume the reference-frame of the link to be  $O_2$  UVW. The link is rotated by 90<sup>0</sup> about X-axis, -90<sup>0</sup> about the –W axis, translated by a distance of 2 units about the Y-axis and finally, rotated by 90<sup>0</sup> about the U axis. Find the resultant homogeneous transformation matrix and the final position (P<sub>2</sub>) of the given end-point.
- 1C. Find the Euler-I and Euler-II angles for the rotation matrix given below; assuming each angle  $\theta \in (0,\pi)$

$${}^{0}R_{E} = \begin{bmatrix} 0.1 & 0.23 & 0.5 \\ 0.5 & 0.866 & 0.5 \\ 0.866 & 0.5 & 1 \end{bmatrix}$$

(2+4+4)

- 2A. With a relevant schematic diagram, explain Impedance Control for robot manipulators.
- 2B. Obtain the forward kinematics equation of the 4 DoF SCARA robot shown in Fig. Q2B.
- 2C. Derive the dynamic model of a planar 2dof RIR arm using Lagrangian algorithm. Assume that the mass of each link is a point-mass located at the centre of mass of each link, and the links are assumed to be rigid, slender structures.

(2+3+5)

- 3A. Give a brief description on any FOUR types of mechanical grippers (with relevant diagrams) based on the type of kinematic device used to actuate finger-movements.
- 3B. Prove that the overall differential transformation of a rigid body in 3-D space due to three differential rotations  $\delta_x$ ,  $\delta_y$  and  $\delta_z$  about X, Y and Z axes (respectively) is independent of the sequence in which these rotations are made.

Table O2C

3C. The DH table for an R-P-R arm is given as follows:

Table Q3C.				
<u>θ</u>	<u>d</u>	<u>a</u>	<u>α</u>	<u>Comment</u>
$\theta_1$			π/2	${}^{0}T_{1}$
	d <sub>2</sub>	1		${}^{1}T_{2}$
θ3		1	π/2	$^{2}T_{E}$

- (i) Obtain the Jacobian matrix, J
- (ii) Determine the possible joint configuration(s) corresponding to kinematic singularity

(iii) If the respective joint-configuration is given by the joint-space,  $q = \left[\frac{\pi}{6} \quad 0.5 \quad \frac{-\pi}{3}\right]^T$  and the

joint velocities by  $\dot{q} = \left[\frac{\pi}{3} \quad 0.3 \quad \frac{-\pi}{6}\right]^T$ , determine the translational and angular Cartesian velocities.

- 4A. Give a brief note on each of the following control scheme (with relevant diagrams):
  - (i) Computed Torque/Force Control
  - (ii) Hybrid Position/Force Control
- 4B. For the 3DoF manipulator arm shown in Fig. Q4C, design a trapezoidal velocity profile for the second revoluting joint. The initial and final positions of the end effector (E) are expressed by the given homogeneous transformation matrices T<sub>s</sub> and T<sub>G</sub> respectively. The time taken for traversal is 4 seconds.

$$T_{s} = \begin{bmatrix} 0.354 & 0.866 & -0.354 & -0.106 \\ -0.612 & 0.5 & 0.612 & 0.184 \\ 0.707 & 0 & 0.707 & 0.212 \\ 0 & 0 & 0 & 1 \end{bmatrix} T_{G} = \begin{bmatrix} 0.583 & -0.766 & 0.272 & 0.027 \\ 0.694 & 0.643 & 0.324 & 0.032 \\ -0.423 & 0 & 0.906 & 0.091 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

(4+6)

(2+3+5)

5A. The code for a MATLAB function 'inverse' given below is found to be erraneous. This function is supposed to find the inverse of a 4×4 homogeneous transformation matrix T. Identify the bug(s) in the code and correct the same.

- 5B. List the various types of position and velocity sensors used in robots.
- 5C. Derive the expressions for designing Discrete Kalman Filter for the linear stochastic discrete-time process given below:

$$\begin{split} \boldsymbol{X}_k &= \boldsymbol{A}_{k-1} \boldsymbol{X}_{k-1} + \boldsymbol{w}_{k-1} \\ \boldsymbol{Y}_k &= \boldsymbol{H}_k \boldsymbol{X}_k + \boldsymbol{v}_k \end{split}$$

where  $w_{k-1}$  and  $v_k$  are assumed to be the process and measurement noises respectively.

(1+3+6)

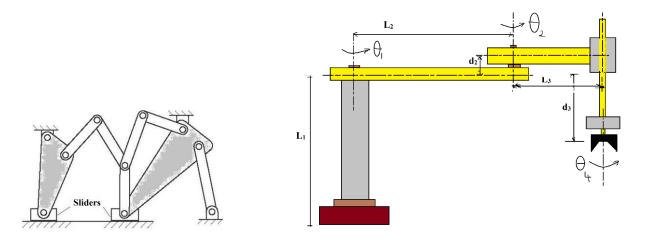


Fig. Q1A

Fig.Q2B

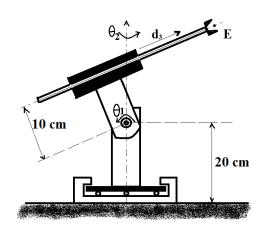


Fig.Q4C

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