Exam Date & Time: 25-Jul-2022 (09:00 AM - 12:00 PM)



## MANIPAL ACADEMY OF HIGHER EDUCATION

## VI SEMESTER B.TECH MAKE UP EXAMINATIONS, JULY 2022

DESIGN AND DRAWING OF CHEMICAL PROCESS EQUIPMENT [CHE 3251]

A

Marks: 50

## Answer all the questions.

Section Duration: 180 mins

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Instructions to Candidates: Answer ALL questions Missing data may be suitably assumed

- 1) A cylindrical pressure vessel 1.8 m outer diameter and 5 m in height is subjected to an internal pressure of 8 kg<sub>f</sub>/cm<sup>2</sup>. Corrosion allowance is 2 mm. What will be the minimum thickness of the vessel if the vessel is fabricated as Class A vessel (J = 1), Class B vessel (5)
  - A) (J = 0.85), Class C vessel (J = 0.5 & J = 0.7). Take allowable stress of the material = 1400 kg<sub>f</sub>/cm<sup>2</sup>.
  - B) The pressure inside an evaporator (1.2 m ID & 46 m height) is 200mmHg. The design temperature is 250°C. Your boss proposes that the wall thickness of this evaporator be 12mm. Check whether this is sufficient or not. (5)
- A pressure vessel has inside diameter 1470 mm and a plate thickness of 5mm. Inside diameter of flange is 1482 mm. A gasket is provided over the flange face. Gasket factor is 2.0 and the gasket seating stress is 120 kg<sub>f</sub>/cm<sup>2</sup>. Inside diameter of gasket is 1485 mm.
  A)
  - Pressure inside the vessel is  $2.5 \text{ kg}_{\text{f}}/\text{cm}^2$ . Permissible stress of flange material is 1060 (5)  $\text{kg}_{\text{f}}/\text{cm}^2$ . Permissible stress in bolts under atmospheric condition is 600  $\text{kg}_{\text{f}}/\text{cm}^2$ . Permissible stress in bolts at operating conditions is 550  $\text{kg}_{\text{f}}/\text{cm}^2$ . Diameter of bolt is 20 mm. Check whether the gasket width is sufficient to keep it away from crushing out.
  - B) While doing thermal design of a 1-2 STHE you end up with the following results: Length of tubes = 5m; No. of tubes = 400; Shell ID = 600 mm;  $\Delta P_t = 65 \text{ kN/m}^2 \& \Delta P_s = 10 \text{ kN/m}^2$ ; Available  $U_{OD} = 500 \text{ W/m}^2\text{K}$ ; Required  $U_{OD} = 2000 \text{ W/m}^2\text{K}$ . Do you feel (5) that this design is satisfactory? If not, what are the strategies will you incorporate to satisfy the design criteria?
- 3) 1-1 STHE is used to heat an organic liquid, which passes through the tubes (30 steel tubes; 5cm ID; 5mm thick) of the exchanger. The density, viscosity, heat capacity and the thermal conductivity of the organic liquid are the same as water (1 g/cc; 1cP; 4.2
  - A) kJ/kg K and 0.54 W/ m K respectively). The shell-side fluid is water that enters with the maximum linear shell-side fluid velocity of 0.15 m/s. determine the shell side heat transfer coefficient.

Shell side: (Take Diameter = OD of tubes):  $Nu = 0.26 \text{ Re}_{max}^{0.6} \text{Pr}^{0.33}$ ;  $G_{max} = (v_{max} * \rho)$ 

B) 1-1 STHE is used to heat an organic liquid  $(50m^3/h)$  from 10°C to 28°C, which passes (5)

4)

A)

through the tubes (30 steel tubes; 5cm ID; 5mm thick) of the exchanger. The density, viscosity, heat capacity and the thermal conductivity of the organic liquid are the same as water (1 g/cc; 1cP; 4.2 kJ/kg K and 0.54 W/ m K respectively). The shell-side fluid is water that enters with flow rate  $3x10^4$  kg/h and temperature 60°C.

Determine the tube side heat transfer coefficient. If the overall heat transfer coefficient is  $500 \text{ W/m}^2\text{K}$ , determine the length of the tubes.

A water-cooled, 1-1 shell-and-tube freon condenser with in-tube condensation of R-22 @37°C has to be designed. City water (Inlet and outlet temperatures are 18°C & 26°C respectively) is used as coolant. The physical properties at the average temperature of the coolant are:  $c_{pL} = 4.181 \text{ kJ/kg K}$ ; viscosity<sub>(L)</sub> = 959x10<sup>-6</sup> Pa.s;  $k_L = 0.606 \text{ W/m K}$ ; Pr = 6.61.

Determine the

• Shell side heat transfer coefficient

(5)

- Overall heat transfer coefficient if the tube side heat transfer coefficient is 157 W/  $m^2 K.$ 

Design parameters:

Design cooling load: 125 kW; One tube pass; Pitch: 1" Square; Shell dia: 15.25"; Baffle Spacing: 35 cm; Number of Tubes: 137; Size of tubes: 0.75" OD & 0.68" ID; Vapor quality = 50%.

B) A water-cooled, 1-1 shell-and-tube freon condenser with in-tube condensation of R-22  $@37^{\circ}C$  ( $c_pL = 1.305 \text{ kJ/kg K}$ ;  $v_L = 8.3734 \times 10^{-4} \text{ m}^3/\text{kg}$ ;  $v_g = 0.01643 \text{ m}^3/\text{kg}$ ; viscosity(L) = 1.86x10<sup>-4</sup> Pa.s; viscosity(g)= 1.39x10<sup>-5</sup> Pa.s;  $k_L = 0.082 \text{ W/m K}$ ; latent heat = 169 kJ/kg; Pr = 2.96) has to be designed. City water (Inlet and outlet temperatures are 18°C & 26°C respectively) is used as coolant. Determine the

- Tube side heat transfer coefficient using Shaw theory. (5)
- Length of the condenser if the overall heat transfer coefficient is  $142 \text{ W/m}^2\text{K}$ .

Design parameters:

Design cooling load: 125 kW; One tube pass; Pitch: 1" Square; Shell dia: 15.25"; Baffle Spacing: 35 cm; Number of Tubes: 137; Size of tubes: 0.75" OD & 0.68" ID; Vapor quality = 50%.

5) A forward-feed evaporator (triple effect) is used to evaporate a solution. Saturated steam at 8.5 atm abs is being used. The feed rate enters at 16°C. Take

A)  $delT_1 = 28 \text{ K}, delT_2 = 23 \text{ K} \text{ and } delT_3 = 42 \text{ K}.$ 

- Determine enthalpy of steam, vapor and liquid streams of each evaporator:
- B) A forward-feed evaporator (triple effect) is being used to evaporate a solution containing 10 wt% solids to a concentrated solution of 50 wt%. The feed rate is 22680 kg/h at 26.7°C. Using the following enthalpy values, calculate the steam and liquid flow rates of each (5) evaporator.

(5)

Enthalpies of each stream		
Steam Enthalpies,	Vapor Enthalpies,	Liquid Enthalpies,
kJ/kg	kJ/kg	kJ/kg
		$@T_F, h_F = 111.95$
$@T_{sl}, \lambda_{s1} = 2199.35$	$@T_I, H_1 = 2684$	$@T_{l}, h_{L1} = 440.21$
$@T_{l}, \lambda_{s2} = 2243.18$	$@T_2, H_2 = 2654.62$	$@T_2, h_{L2} = 364.35$
$@T_2, \lambda_{s3} = 2290.27$	$@T_3, H_3 = 2600.9$	$@T_3, h_{L3} = 230.24$

## Useful Energy Balance Equations:

- $F(h_{F}|-H_{1}) + S\lambda_{s1} = L_{1}(h_{L1}-H_{1})$
- $L_1 (h_{L1} \lambda_{s2} H_2) + F \lambda_{s2} = L_2 (h_{L2} H_2)$
- $L_2 (h_{L2} \lambda_{s3} H_3) + L_1 \lambda_{s3} = L_3 (h_{L3} H_3)$

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