MANIPAL INSTITUTE OF TECHNOLOGY MANIPAL REDEN

(A constituent unit of MAHE, Manipal)

DEPARTMENT OF ELECTRICAL & ELECTRONICS ENGINEERING

I SEMESTER M.TECH. (POWER ELECTRONICS & DRIVES) END SEMESTER EXAMINATIONS, NOVEMBER-DECEMBER 2023

MODELLING OF ELECTRICAL MACHINES [ELE 5115]

REVISED CREDIT SYSTEM

Time: 3 Hours	Date: 07 December 2023	Max. Marks: 50
Instructions to Candidates:		
 Answer ALL the questions 	5.	

- Missing data may be suitably assumed.
- Derive the magnetic energy stored as a function of plunger position x' for **1A**. a relay shown in Fig Q(1A). N=1500, g=2 mm, d=0.15 m, l=0.1 m & i=5 A. Assume h >> q.

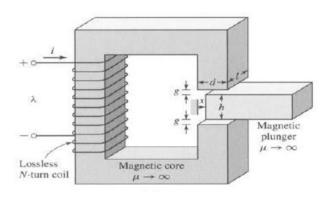


Fig. Q(1A)

- **1B**. Consider a nonlinear magnetic system with cylindrical motion. Derive an expression for Torque using (i) Field-energy method and (ii) Co-energy method.
- **1C**. The inductance of a solenoid as a function of displacement x is given by $L(x)=0.15x^{4}-1.1x^{3}+2.86x^{2}-3.5x+2.8$

Calculate the force acting on the solenoid for an exciting current of 0.75A. (03)

- 2A. With the help of neat diagrams, show that the rotor self-inductance of a constant airgap machine is independent of rotor position. (03)
- 2B. With neat diagrams, derive an expression for self-inductance of a salient pole rotor. (03)
- **2C**. Obtain the transformation matrix to transform 3-phase variables to 2phase variables using (i) power invariance and (ii) power variance approach. (04)

(04)

(03)

- 3A. The following are the 3-phase ac voltages $v_a=220sin\omega t$, $v_b=220sin(\omega t-$ 120°) & $v_c = 220 \sin(\omega t + 120°)$. Transform these voltages to (i) stationary frame and (ii) rotating dg frame.
- 3B. Consider the dynamic model of a 3-phase induction motor in the stationary reference frame.

0

...0

$$\begin{split} V_{\alpha\beta}^{\alpha\beta} &= RI_{\alpha\beta}^{\alpha\beta} + L\frac{d}{dt}I_{\alpha\beta}^{\alpha\beta} + GwI_{\alpha\beta}^{\alpha\beta} \text{ where} \\ L &= \begin{bmatrix} l_{ls} + 1.5L_{ms} & 0 & 1.5M_{sr}cos\theta & -1.5M_{sr}sin\theta \\ 0 & l_{ls} + 1.5L_{ms} & 1.5M_{sr}sin\theta & 1.5M_{sr}cos\theta \\ 1.5M_{sr}cos\theta & 1.5M_{sr}sin\theta & l_{lr} + 1.5L_{mr} & 0 \\ -1.5M_{sr}sin\theta & 1.5M_{sr}cos\theta & 0 & l_{lr} + 1.5L_{mr} \end{bmatrix} \& \\ G &= \begin{bmatrix} 0 & 0 & -1.5M_{sr}sin\theta & -1.5M_{sr}cos\theta \\ 0 & 0 & 1.5M_{sr}sin\theta & -1.5M_{sr}cos\theta \\ -1.5M_{sr}sin\theta & 1.5M_{sr}cos\theta & 0 & 0 \\ -1.5M_{sr}cos\theta & -1.5M_{sr}sin\theta & 0 & 0 \end{bmatrix} \end{split}$$

Derive the dynamic model of the machine in pseudo-stationary reference frame.

- 4A. Develop a small signal model of a separately excited dc motor with field voltage, armature voltage and load torgue as inputs and field current, armature current and speed as the outputs. Also derive the transfer function $\Delta \omega_r(s) / \Delta V_a(s)$.
- **4B**. Analyze the behaviour of q-axis equivalent circuit diagram of a salient pole synchronous machine with $S\psi_{as}(s)$ as output & $I_{as}(s)$ as the input.
- Consider the machine coils shown in Fig Q(5A). By observation, write the 5A. dynamic equations of a salient pole synchronous machine and hence develop the equivalent circuit diagrams of d-axis & q-axis in synchronous reference frame.

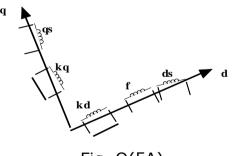


Fig. Q(5A)

5B. With the help of phasor diagram of an under-excited salient pole synchronous machine, show that the active power

$$P = \frac{EV_a \sin\delta}{x_{ds}} - \frac{EV_a \sin 2\delta}{2} \left(\frac{1}{x_{qs}} - \frac{1}{x_{ds}}\right)$$
(03)

5C. Compare the working principle of permanent magnet synchronous machine and synchronous reluctance machine. (03)

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